

Maximizing Brown Field Production In High Artificial Lift Failures Frequency Environment As A Result Of Wells Harsh Conditions

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"Go to Green-Sustain Oil Gain"







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Field Overview								
Location	350 Sq. Km, Eastern Desert							
Operators	KEE, 70% WI, 30% WI for PETROGAS.							
Running wells	59							
Producing Res.	HF (50%), Yusr (21%), Kareem (12%) & others(17%)							



AREA-A Reservoir Parameters:

- Very Low Pressures down to 100 PSI; with average pressure in HF with 150 PSI, and 500 PSI in Yusr reservoirs; Average depths is 700 Mt. for HF reservoir and 1100 Mt. for Yusr reservoirs.
- Very High Conductivity of PI 20 BBD/PSI; with maximum production of 1800 BBL/Day in HF reservoir.
- Average Associated gas with oil is 100 KSCFD.

Introduction: AREA-A Wells

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Challenges and Harsh Conditions

Sever Sand Production

- Due to Depletion, shallow depths, and high conductivity; severe sand production encountered with non uniform sand sorting;

COARSE FINE MEDIUM

• Depletion

- Average reservoir pressure in AREA A fields is relatively very low down to 100 PSI
- Due to Depletion; increase the need to run as deep as possible near to perforations or below perforations; thus, increase of pump sticking troubles due to sand production



High Conductivity Reservoirs

- Estimated PI of SHNW area about 10 BBD/PSI; however, of the depletion encountered, the reservoir AOF could be 1900 BBL/Day
- Difficulties of running ESP at these levels of very low reservoir pressure with associated high GOR and severe sand production; which require another new techniques of Artificial lifting methods to produce such high rates

Old/Loose Integrity Wells

- AREA-A Fields is old fields since 1950's; thus, led to lose integrity CSG and obsolete CSG Weights; thus, requires special equipment specifications (i.e., 7", 20 IB/Ft. Packers)

Challenges Mitigations Techniques AREA-A Sand Production Solutions Scenarios





Classification: Internal



AREA-A Sand Production Solutions "High Clearance Pumps"

High Clearance Pump Technique:

Increase clearance between Plunger and barrel from current standard value of -0.003 & -0.005 to higher value of -0.009 or more up to -0.011

Increase Clearance reduces risk of Plunger sticking with barrel; but cause production drop due to increase slippage **Technique Applications Basis**

- AREA-A Wells Produces from relevant shallow depths 700 to 1200 Mt.; which induces hydrostatic pressure of average of 1500 PSI
- AREA-A Wells running with excessive high parameters and large bore size pumps which compensate any production drop due oil slippage







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AREA-A Sand Production Solutions "High Clearance Pumps"

Oil Slippage Calculations Basis

Viscosity in Centipoise, at temperature (°F) and API gravity															
API GRAVITY	60°	70 °	80 °	90°	100°	120°	140°	160°	180°	200°	220 °	240°	260°	280°	300°
14	5000	3000	2000	1000	750	300	190	80	52	33	24	17	12	9	8
19.8	350	250	180	140	100	60	40	27	19	14	11	8.7	6.8	5.8	5
26.8	49	38	29	23	19	13	9.5	7	5.8	4.5	3.7	3.2	2.8	2.4	2.1
31.1	12.5	10	8.8	7.4	6.5	5	4.1	3.3	2.8	2.4	2.1	1.9	1.6	1.5	1.3
34.6	7.8	6.4	5.5	4.5	4	3.3	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1	0.9
44	3.3	3	2.7	2.4	2.2	1,9	1.7	1.4	1.3	1.2	1.1	0.9	N/A	N/A	N/A

Plunger Diameter, inches Plunger seal Length, inches Fluid Level from Surface, feet Specific Gravity of Fluid



(Enter these four data items, then read slippage below by choosing viscosity and clearance.) (If needed, a viscosity conversion chart is below)

Slippage in Barrels per Day											
Clearance	Viscosity in Centipoise μ										
inches C	1	2	4	8	16	32	64	128	256	512	1028
0.001	0.73	0.36	0.18	0.09	0.05	0.02	0.01	0.01	0.00	0.00	0.00
0.002	2.09	1.05	0.52	0.26	0.13	0.07	0.03	0.02	0.01	0.00	0.00
0.003	3.87	1.94	0.97	0.48	0.24	0.12	0.06	0.03	0.02	0.01	0.00
0.004	6.00	3.00	1.50	0.75	0.38	0.19	0.09	0.05	0.02	0.01	0.01
0.005	8.42	4.21	2.11	1.05	0.53	0.26	0.13	0.07	0.03	0.02	0.01
0.006	11.11	5.56	2.78	1.39	0.69	0.35	0.17	0.09	0.04	0.02	0.01
0.007	14.05	7.02	3.51	1.76	0.88	0.44	0.22	0.11	0.05	0.03	0.01
0.008	17.21	8.60	4.30	2.15	1.08	0.54	0.27	0.13	0.07	0.03	0.02
0.009	20.58	10.29	5.15	2.57	1.29	0.64	0.32	0.16	0.08	0.04	0.02
0.010	24.16	12.08	6.04	3.02	1.51	0.75	0.38	0.19	0.09	0.05	0.02
0.011	27.92	13.96	6.98	3.49	1.75	0.87	0.44	0.22	0.11	0.05	0.03
0.012	31.87	15.94	7.97	3.98	1.99	1.00	0.50	0.25	0.12	0.06	0.03
0.013	35.99	18.00	9.00	4.50	2.25	1.12	0.56	0.28	0.14	0.07	0.04
0.014	40.29	20.14	10.07	5.04	2.52	1.26	0.63	0.31	0.16	0.08	0.04
0.015	44.74	22.37	11.19	5.59	2.80	1.40	0.70	0.35	0.17	0.09	0.04
0.016	49.35	24.68	12.34	6.17	3.08	1.54	0.77	0.39	0.19	0.10	0.05
0.017	54.12	27.06	13.53	6.76	3.38	1.69	0.85	0.42	0.21	0.11	0.05
0.018	59.03	29.51	14.76	7.38	3.69	1.84	0.92	0.46	0.23	0.12	0.06
0.019	64.08	32.04	16.02	8.01	4.01	2.00	1.00	0.50	0.25	0.13	0.06
0.020	69.28	34.64	17.32	8.66	4.33	2.16	1.08	0.54	0.27	0.14	0.07
0.021	74.61	37.31	18.65	9.33	4.66	2.33	1.17	0.58	0.29	0.15	0.07
0.022	80.08	40.04	20.02	10.01	5.00	2.50	1.25	0.63	0.31	0.16	0.08
0.023	85.68	42.84	21.42	10.71	5.35	2.68	1.34	0.67	0.33	0.17	0.08
0.024	91.40	45.70	22.85	11.43	5.71	2.86	1.43	0.71	0.36	0.18	0.09

Estimating the oil viscosity from the below table: It was concluded that AREA wells viscosity is about 5 to 13 CP

Depleted High Conductivity Reservoirs "Sucker Rod Over Sized Pumps"

3.25" OTP Pump

Non-Conventional oversized pump; able to produces rates from 500 BFPD to 1900 BFPD; in Shallow depths (700 Mt. up to 1100 Mt.), in depleted wells of 150 PSI reservoir pressure.

Normally 3.25" DHP is designed to be run inside 4.5" TBG; but due to non availability of this TBG size in AREA-A Inventory, an innovative idea to run this type of pumps inside 3.5" EUE TBG; which is On-Off Tool

<u>Sucker Rod Pump On-Off Tool</u>; is a designed tool to connect rod string with down hole pump plunger

Running Procedures "Idea" of the OTP Pump inside 3.5" EUE TBG

- 1. Since Plunger size is 3.25" which couldn't be run inside 3.5" EUE TBG "2.99" ID"; the barrel is connected to TBG and ran separately with the TBG String, and the plunger is left inside the barrel while RIH
- 2. The Plunger is being run with bottom part of the On-Off Tool; and to be ready for attachment with top part of the On-Off Tool
- 3. Top Part of On-Off Tool is being run with sucker rod string
- 4. Once Sucker Rod String being run inside the TBG; Slacking the top part of On-Off Tool on the bottom part with slight rotation till fully connected



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Depleted High Conductivity Reservoirs "Sucker Rod Over Sized Pumps"





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Placing More Than One Pump in Same Completion"

Placing More than Pump Sizes in Same Completion

As result of Harsh Conditions "Sand, & Corrosion" which requires back up option to produce the well instantaneous once the pump failed due to the following reasons

- 1. Well Productivity is sufficiently high; and might affect the area production
- 2. TBG Leak just above the bottom pump
- 3. Sucker Rod TBG Pump barrel corrosion or erosion; and rig is not available

<u>Methodology</u>

In case completed the well with TBG Pump i.e. 2.75", placing pump seating nipple two joints above the TBG Pump to provide a back up option in case pump failed for any reason

In Key important wells; which is running with 3.25" OTP Pumps; completed with two contingent plans; hence the well is running with 3.25" OTP Pumps, with 2.75" TBG Pump barrel on joint above the OTP Pump, then 2.25" Pump Seating nipple placed two joints above the 2.75" TBG Pump.



Depleted High Conductivity Reservoirs "Sucker Rod Over Sized Pumps"



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Results and Conclusion

Mean Time Between Failures (MTBF) & Mean Time to Recover

(MTTR)



MTBF & MTTR, Wells WO



MTBF & MTTR, Wells WO

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Since Application of the Mitigation Techniques; Observed

- Enhancement of MTBF from 215 Days in 2022 up to 451 days as an average of first half of 2023 1.
- Enhancement of MTTR from 1.8 days in 2022 down to 1.3 days as an average of first half of 2023 2.

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Summary and Recommendations

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1- Selection of Optimum method to handle sand production troubles based on Area Experience and challenge all possible solution based on studies, trials, grab data, and execution on all area wells

2- Oversized Sucker Rod Pumps with the On-Off Tool provides affordable method to produce high-rate low pressure reservoir in a depleted gassy, and sandy environment which ESP couldn't handle & not cost effective

3- In Shallow depleted reservoir utilization sucker rod pump with high clearance provide excellent solution rather than costly gravel pack which induces additional pressure drop on such very depleted reservoirs

4- Internal Resources utilization to provide back up options in Key problematic wells is essential which revealed in utilization of more than one pump size in the same well to provide many back up options to return failed wells to production ASAP.



THANK YOU

classification refurther information Please access the SPE paper: SPE- 216432-MS